GEOTECHNICAL REPORT

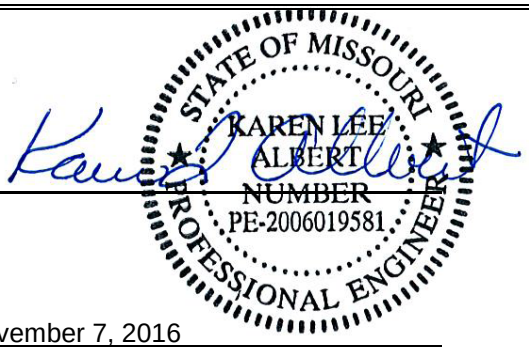
Scenic Regional Library
Wildcat Lane
Wright City, Missouri

Project No. 16-6414

November 2016

Presented to:

Scenic Regional Library



November 7, 2016
Date

Karen L. Albert, P.E. #2006019581
State of Missouri
Registered Professional Engineer for Cochran

COCHRAN

Architecture • Civil Engineering • Land Surveying • Site Development • Geotechnical Engineering • Inspection & Materials Testing

8 East Main Street
Wentzville, Missouri 63385
Telephone: 636-332-4574
Fax: 636-327-0760

737 Rudder Road
Fenton, Missouri 63026
Telephone: 314-842-4033
Fax: 314-842-5957

530A East Independence Drive
Union, Missouri 63084
Telephone: 636-584-0540
Fax: 636-584-0512
www.cochraneng.com

201B West Karsch Boulevard
Farmington, Missouri 63640
Telephone: 573-315-4810
Fax: 573-315-4811

905 Executive Drive
Osage Beach, Missouri 65065
Telephone: 573-525-0299
Fax: 573-525-0298

November 7, 2016

Mr. Steve Campbell, Director
Scenic Regional Library
304 Hawthorne Drive
Union, Missouri 63084

RE: Geotechnical Investigation
Scenic Regional Library
Wildcat Lane
Wright City, Missouri
Project No. 16-6414

Dear Mr. Campbell:

Attached is our Geotechnical Report presenting the results of a subsurface exploration conducted for the above-referenced project. This exploration was conducted in general accordance with our proposal. The Geotechnical Report includes our understanding of the project, observed site conditions, conclusions and/or recommendations, and support data as listed in the Table of Contents.

We appreciate the opportunity to be of service to you on this project. We welcome the opportunity to provide other services during the course of the project, should they be necessary. If you have any questions or comments, please feel free to contact us.

Sincerely,

Karen L. Albert, P.E.
Director of Geotechnical Services
Cochran

Copies submitted: 3 Bound Reports, 1 Electronic

TABLE OF CONTENTS

1. EXECUTIVE SUMMARY

The following is a brief summary of the exploration including our findings, conclusions, and recommendations. The summary omits a number of details, any one of which could be crucial to the proper application of this report. Any party who relies on this report must refer to subsequent sections within the report for a more detailed discussion.

A. The project consists of an approximately 7,700 square foot, one-story, slab-on-grade structure with associated parking and driveways.

B. The soil stratigraphy at the site generally consists of medium stiff to very stiff, medium to high plastic clay to the boring termination depth. Auger refusal was not encountered in the six borings.

C. The proposed structure may be supported on strip and spread footings proportioned for a net allowable bearing pressure of 2,000 pounds per square foot (psf), provided the footings bear on natural firm soil or engineered fill.

D. Care must be exercised to maintain the integrity of the subgrade during grading, as the soils are susceptible to disturbance.

E. Expansive soil is present at the site that will affect the proposed construction. Over excavation and replacement of the medium to high plastic soils is recommended to reduce the risk of foundation and floor slab distress.

2. INTRODUCTION

Cochran has completed the requested geotechnical service for the proposed one story, slab-on-grade structure located on the west side of Wildcat Lane near the intersection of Wildcat Lane and Browning Drive in Wright City, Missouri. The services documented in this report were provided in accordance with the terms, conditions and scope of services described in Cochran's proposal. This report was prepared for the purpose of describing the subsurface conditions at the site, analyze and evaluate the test data, and develop recommendations for geotechnical aspects of the design and construction of the project. Our services consisted of site reconnaissance, drilling six borings, laboratory testing, engineering analyses, report preparation and submittal of this report.

3. PROJECT AND SITE DESCRIPTION

The project will include the construction of an approximately 7,700-square foot, one-story, slab-on-grade structure with associated driveways and parking. The structure will be constructed on the west side of Wildcat Lane near the intersection of Wildcat Lane and Browning Drive in Wright City, Missouri. We understand the finished floor elevation for the planned structure will be approximately EL 750.50. Structural loads were not provided.

Currently the site is grass covered. Based on a topographic survey conducted by Cochran dated April 29, 2016, the elevations at the site within the proposed building footprint ranges from approximately El 747 to 748. The finished floor elevation for the proposed structure will be approximately El 750.50. Fills up to approximately four feet are anticipated within the building footprint. The site location is shown on the United States Geological Survey (USGS) map included as Plate 1.

4. FIELD EXPLORATION AND LABORATORY TESTING

A. Field Exploration. The subsurface conditions at the site were explored by drilling six borings, four (4) within the building footprint (Borings B-1 through B-4) and two (2) within the proposed parking area (Borings B-5 and B-6). The boring locations were located in the field by measuring distances from existing site features. The boring locations are presented on Plate 2. The elevations at the boring locations were interpolated from a topographic survey conducted by Cochran. The locations and elevations should be considered accurate only to the degree implied by the methods employed.

The six borings were drilled to predetermine depths of 10 and 20 feet without encountering auger refusal. Standard Penetration Tests (SPTs) were generally obtained at 2.5-foot and 5-foot intervals in the overburden soils using an automatic hammer. Undisturbed Shelby tube samples were obtained at select locations. The samples were sealed, secured, and transported to our laboratory for observation and testing.

The sampling intervals, soil descriptions, standard penetration data and other pertinent field information are indicated on the boring logs, which are presented in Appendix A. An explanation of the terms and symbols used on the boring logs is also provided in Appendix A.

B. Laboratory Testing. In the laboratory, the samples were observed and described by an engineer using manual-visual methods. Moisture contents were determined for cohesive soil samples. Atterburg limits were determined for select soil samples. Unconfined compressive tests were conducted on select Shelby tube samples. The results of the laboratory tests are presented on the boring logs.

5. SUBSURFACE CONDITIONS

The general description of the soils encountered during the subsurface exploration is presented herein. The stratification lines on the boring logs are approximate and the transition between the materials may be gradual rather than distinct.

A. Stratigraphy. The stratigraphy at the six boring locations at the site generally consist of medium stiff to very stiff, medium to high plastic clay to boring termination depth. The six borings were terminated at predetermined boring depths of 10 and 20 feet without encountering auger refusal.

Topsoil was encountered at a depth of 4 inches in Borings B-1, B-2, B-4, B-5 and B-6.

Atterberg limit tests were performed on three samples of the cohesive soils at depths of approximately 1 to 5 feet. The samples exhibited liquid limits of 41 and 43 with plasticity indexes of 23 and 26.

Atterberg limits tests, used to determine soil plasticity, are summarized in the table below:

Boring No.	*Depth, ft.*	*Liquid Limit*	*Plastic Limit*	*Plasticity Index*
1	1-2.5	43	20	23
2	1-2.5	43	17	26
3	3.5-5	41	15	26

The plasticity index (PI) is the difference between a soil's liquid and plastic limits. Per *Foundation Engineering* (Ralph B Peck, Walter E Hanson, Thomas H. Thornburn, 2nd Edition, 1974), the shrink swell potential of a soil is a function of its PI:

Swell Potential	*Plasticity Index (PI)*
Low	0-15
Medium	10-35
High	20-55
Very High	>35

The results of the Atterberg limits testing of the natural residual clay from Borings B-1, B-2 and B-3 indicated plasticity indexes of 23 and 26, respectively. These PIs generally correspond to a medium to high swell potential.

B. Groundwater. Groundwater was not encountered in the six borings during the subsurface exploration program. It should be understood that the lack of observed groundwater levels on the boring logs may indicate groundwater may not have stabilized prior to backfilling. Groundwater may fluctuate over time due to seasonal and climatic variations. Therefore, the lack of or observed groundwater levels may not represent present or future levels.

6. GEOTECHNICAL CONSIDERATIONS AND RECOMMENDATIONS

The soils at the site are susceptible to disturbance during grading operations (i.e, pumping and/or rutting). Care must be exercised to maintain the integrity of the subgrade when preparing the site for the placement of fill, making excavations, and other earth-related construction activities. If sensitive soils are present, a special approach to grading may need to be adopted. The special approach to grading includes excavating with a

trackhoe or wide-tracked excavator. Care should be exercised to maintain the integrity of the subgrade prior to the placement of fill and building construction.

Medium to high plastic soils were encountered in the six borings at depths that will affect the proposed construction (EL 746 to EL748). The finished floor elevation for the proposed structure will be EL 750.50. The expansive clay soils have the potential for volume change with corresponding changes in the soil moisture content. The volume change can lead to movement and cracking of floor slabs and in severe cases, movement and cracking of foundations and walls. Therefore, remediation of the expansive clay soils to a minimum depth of 5 feet (EL 745 - based on a finished floor elevation of EL 750.5) below the finished floor elevation is recommended within the proposed building footprint.

A. Site Preparation. All vegetation/organic materials must be stripped where encountered. The organic material can be stockpiled on-site for later use in landscaped areas or disposed of off-site in a legal manner. In all areas, the resulting exposed subgrade should be proofrolled, and any soft soil or yielding areas should be over excavated and backfilled with new compacted fill or well-graded crushed rock.

B. Expansive Clay Soil. Medium to high plastic soil (liquid limit greater than 45 percent and/or a plastic index equal to or greater than 20 percent) was encountered in the six borings which will affect the proposed construction (EL 746 to EL 748). In general, expansive clays can cause damage if they exhibit excessive shrink and swell characteristics. Where the bearing and/or subgrade soils consist of expansive clay soils, we recommend that they be removed to a minimum depth of 5 feet (EL 745 – based on a finished floor elevation of EL 750.5)) below the finished floor elevation. The overexcavation should extend at least 5 feet beyond the outside edge of the building footprint to facilitate uniform compaction of the replacement materials and may require additional widening at the corners to allow equipment access for proper compaction. The overexcavation should be backfilled with properly compacted low plastic soil or 1-inch minus crushed limestone or limestone screenings. The foundations and floor slabs would then be constructed on the newly placed fill.

   Although not required, it is advised remediating highly plastic soil in sidewalk and pavement subgrade to a depth of 8 inches below proposed subgrade elevation.

C. Fill Materials. Prior to placement of the fill, the fill material is to be approved by a representative of Cochran. In general, fill materials should consist of low plasticity, (liquid limit less than 45 percent and a plasticity index less than 20) cohesive soils or granular materials. Acceptable non-organic fill soils include materials designated CL, ML, CL-ML, SP, SW, and GW by ASTM D 2487. Open-graded “clean” granular materials, in general, should not be used, as they tend to hold water, resulting in softening of the underlying cohesive soil subgrade.

D. Compaction. Fill or backfill must be placed in lifts of uniform thickness and compacted. The fill should be placed in 8-inch loose lifts. The engineered fill should be compacted to at least 95 percent of its standard Proctor (ASTM 698) maximum dry density and be placed at a moisture content that is plus or minus 2 percent of optimum moisture content. The soil fill may require aeration or wetting at the time of construction to achieve proper compaction. Deleterious material should not be included in fill, nor should the fill be placed on soft or frozen materials.

   Settlement of loosely backfilled utility trenches can result in unsightly depressions and localized pavement failures. The magnitude of settlement can be significantly reduced by mechanically compacting the trench backfill to the minimum specified compaction levels given in the Compaction Section.

   Observation of the type of soil or granular material to be placed as fill, placement of the compacted fill and field density testing should be performed by a qualified technician on each lift to verify the compaction requirements are met in the field and to insure that high plastic or highly compressible soils are not in the fill within the building pad area.

E. Site Drainage and Grading. During construction, proper drainage should be provided to protect the foundation excavations, floor slab and pavement subgrades from the detrimental effects of weather conditions during construction. Finished subgrades and foundation excavations should be kept free of standing water at all times.

   Positive site drainage should be provided to reduce surface water infiltration around the perimeter of the building and beneath the floor slab. Grades must be sloped away from the structures and roof and surface

drainage collected and discharged in such a way that water is not permitted to infiltrate the foundation backfill. Drain and utility pipes beneath the floor should have tight joints to prevent leakage. Utility trenches beneath the floor slab and pavement areas should be carefully backfilled with compacted low plastic soil or minus gradation crushed rock. "Clean" rock backfill can be a possible pathway for moisture to the potentially expansive high plastic clay.

Large trees and shrubs should not be planted next to exterior footings as they may cause drying and shrinkage of the foundation soils and, with the passage of time, potentially detrimental settlement of the building floor slab and foundation may occur. A minimum distance of 20 feet or a distance equal to 1.5 times their expected mature height is suggested.

7. FOUNDATIONS

Shallow foundations bearing on firm natural soil or engineered fill are appropriate for support of the proposed building. Strip and spread footings may be proportioned for a net allowable bearing pressure of 2,000 pounds per square foot (psf).

The minimum lateral dimensions for strip and spread footings should be 24 and 30 inches, respectively. Exterior footings should be embedded 30 inches below the lowest adjacent exterior grade for frost protection purposes. Due to the periodic severity of winters in this area, footings in poorly heated or unheated areas of the building should also be placed at least 30 inches below the adjacent exterior grade. All footings must be protected from the effects of frost when construction is carried out during winter months.

The bearing conditions at the base of the footing excavation should be observed by Cochran personnel. The base of all foundation excavations should be free of water and loose soil prior to placing concrete.

8. FLOOR SLABS

The floor slabs should be underlain by a minimum 4-inch layer of well-graded crushed rock to distribute concentrated loads and reduce potential capillary moisture transfer. The use of a plastic vapor barrier is left to the discretion of the architect. Careful attention to curing of the concrete slabs should be followed if a polyethylene moisture barrier is placed on top of the crushed stone and beneath the floor or excessive shrinkage cracking and "curling" may occur.

The floor slabs should be designed to allow for differential movements, which normally occur between the floor slab, columns and foundation walls. Joints should be placed in the floor slab in accordance with the applicable American Concrete Institute (ACI) standards and be located in such a manner that each floor slab section is rectangular. Such joints permit slight movements of the independent elements and help prevent random cracking that might otherwise be caused by restraint of shrinkage, slight rotations, heave, or settlement.

9. SEISMICITY

The International Building Code (IBC) requires the structural design of the proposed building to be in accordance with the appropriate seismic intensity zoning requirement. Per the general procedures of Section 1615.1 of the 2009 edition of the IBC, the soil profile at the project site may be defined as Class C. This designation is based on the results of the borings and our local knowledge of the geologic conditions in the area. Consequently, 100-foot borings are not required.

10. PAVEMENT CONSIDERATIONS

A pavement analysis and design is beyond the scope of our services. The thickness of the pavement section used is directly related to the service life and the initial costs. The owner's desire may range from a low cost pavement having a short life to a more costly pavement with a longer expected life and less maintenance.

There are certain aspects in the design and construction of pavements that should be considered. The subgrade should be shaped to prevent ponding if pavements are not constructed immediately after grading. Minor ponding, even short durations, can cause softening of a soil subgrade to a significant depth. The pavement subgrades may be subjected to construction traffic and exposure to weather for an extended period. Therefore, it may be necessary to proofroll the subgrade, in both cut and fill areas and recompact the subgrade immediately prior to placing base rock for the pavement. Soft areas should be selectively undercut and backfilled with properly compacted cohesive soil of the same type present in the subgrade, possibly combined with a geotextile

or geogrid. Proofroll passes should be limited, particularly on silty subgrades to reduce the potential for pumping of moisture from deeper within the soil profile. The asphaltic concrete surface course should be checked during placement to verify density and total thickness.

11. RECOMMENDED CONSTRUCTION SERVICES

The conclusions and recommendations given in this report are based on interpretation of exploration data and Cochran's experience. The client must recognize variations may occur from conditions observed in the borings, particularly within existing fills or previously developed areas. The design recommendations are based on data from borings, sampling and related procedures. Actual subsurface conditions may vary from those encountered in the 5 borings. Therefore, design recommendations are subject to adjustment in the field, based on subsurface conditions encountered during construction.

The following list highlights Cochran's recommendation for a construction monitoring program. These services are recommended to provide quality assurance in assessing design assumptions and to document procedures for compliance with plans, specifications, and good engineering practice. Cochran should be retained to:

A. Review grading and foundation plans to observe that recommendations given in this report have been correctly implemented.

B. Assess the suitability of potential fill materials, including both on-site and off-site sources (if applicable)

C. Monitor placement of structural fill and backfill.

D. Observe foundation excavations to verify that suitable bearing materials are present.

E. Observe floor slab subgrades to assess the impact of medium and high plastic clay soils and to recommend the extent of remedial measures.

F. Provide testing services during pavement construction.

Construction observation is intended to enhance compliance with project plans and specifications. It is not insurance, nor does it constitute a warranty or guarantee of any type. In all cases, contractors, etc., are solely responsible for the quality of their work and for adhering to plans and specifications.

12. LIMITATIONS OF REPORT

The recommendations provided herein are for the exclusive use of the client for specific application to the named project as described herein. They are not meant to supersede more stringent requirements of local ordinances. They are based on the subsurface information obtained at six specific borings within the project area, our understanding of the project and geotechnical engineering practice consistent with the standard of care. If this report is provided to prospective contractors, the client should make it clear that the information is provided for factual data only and not as a warranty of subsurface conditions included in this report.

This report does not reflect variations that may occur between borings, across the site, or due to the modifying effects of weather. The nature and extent of such variations may not become evident until, during or after construction. If variations appear, we should be immediately notified so that further evaluation and supplemental recommendations can be provided.

The scope of our services for this phase of the project did not include any environmental assessment or investigation for the presence or absence of wetlands or hazardous or toxic material in the soil, surface water, groundwater or air, on or below or around this site. Any statements in this report or on the soil logs regarding odors noted or unusual or suspicious items or conditions observed are strictly for the information of our client.

Cochran should be provided with a set of final development plans as soon as they are available for review to determine the applicability of our recommendations. Failure to provide these documents may nullify some or all of the recommendations provided herein. In addition, any changes in the planned project or changed site conditions may require revised or additional recommendations on our part.

Cochran should be retained to perform construction observation and complete its geotechnical engineering service using the observational methods. Cochran cannot assume responsibility or liability for the adequacy of its recommendations when they are used in the field without Cochran being retained to observe construction.

ILLUSTRATIONS

VICINITY AND TOPOGRAPHIC MAP

SITE VICINITY MAP
NO SCALE

KLAUSMEIER RD
SCOTT RD
LAKE TUCCI CIR
MARLIN DR
BOBWHITE LN
SPARROW
QUAIL CREEK DR
SPRING HILL CIR
WESTWOODS RD
BRYAN RDG
BELL RD
WILDCAT DR
SITE
Wright City
FREEDOM LN
70
NW 2ND ST
RED LEAF WAY
AUBURN DR
ROTTERS CREEK LN
700

GENERAL NOTES / LEGEND

USGS TOPOGRAPHIC MAP
WRIGHT CITY, MO 2015
20' CONTOURS
GOOGLE MAPS

VICINITY & TOPOGRAPHIC MAP

SCENIC REGIONAL LIBRARY

WRIGHT CITY, MO

N

DWN. BY:	APPD. BY:
JMM	KLA

DATE: AUG. 10, 2016
SCALE: 1"=2000'
PROJ. NO: 16-6414
PLATE: *1*

ILLUSTRATIONS

SITE AND BORING LOCATIONS

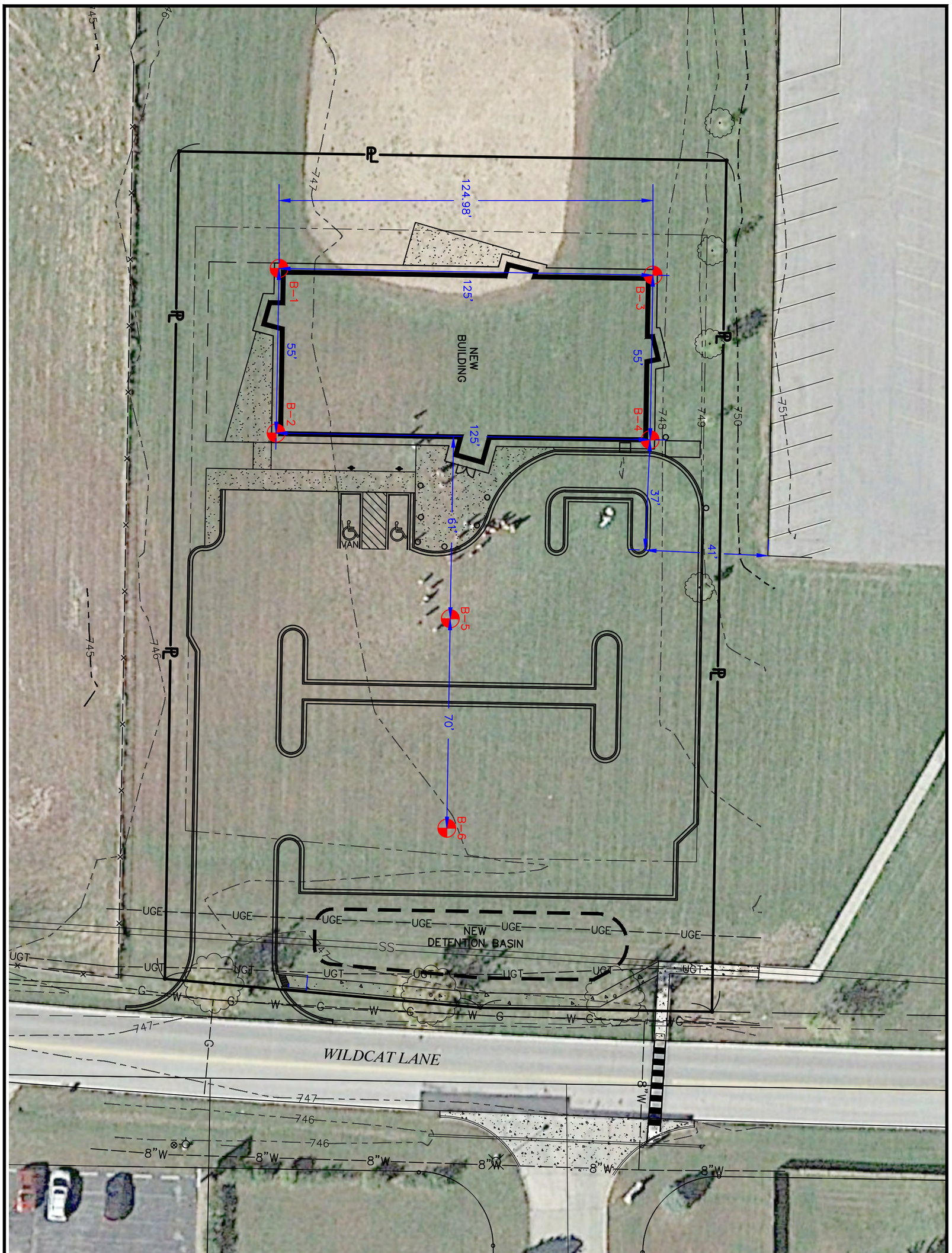


PLATE: 2	DWN. BY: JMM	GENERAL NOTES	*SITE PLAN & BORING LOCATIONS* *SCENIC REGIONAL LIBRARY* *WRIGHT CITY, MO*
PROJ. NO: 16-6414	APP'D. BY: KLA		
SCALE: 1"=30'	DATE: AUG. 10, 2016		

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APPENDIX A

DETAILED LOGS OF BORINGS B-1 THROUGH B-6
BORING LOG: LEGEND AND NOMENCLATURE

LOG OF BORING NO. **B-1**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 20.0 ft

ELEVATION, ft	DEPTH, ft	SYMBOL	DESCRIPTION	SAMPLES	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	PERCENT PASSING NO. 200 SIEVE	SPT N-VALUE blows per foot
			SURFACE ELEVATION: 747.0ft								
747.0	0		TOPSOIL - 4 inches								
746.8			Medium stiff, brown and gray, medium plastic CLAY - CL-CH			27	43	20	23		5
744.0			Medium stiff to very stiff, brown and gray, high plastic CLAY - CH		106	18					
	5					23					8
						21					11
	10										
						18					16
	15										
			trace gravel			17					16
727.0	20		Boring terminated at 20 feet								
	25										

UNDRAINED SHEAR STRENGTH, tsf
○ HAND PENETROMETER
△ TORVANE
● UNCONFINED COMPRESSION
▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL
0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

LOG OF BORING NO. **B-2**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 20.0 ft

ELEVATION, ft	DEPTH, ft	SYMBOL	DESCRIPTION	SAMPLES	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	PERCENT PASSING NO. 200 SIEVE	SPT N-VALUE blows per foot
746.5	0		SURFACE ELEVATION: 746.5ft								
746.3			TOPSOIL - 4 inches								
			Medium stiff to stiff, brown and gray, medium plastic CLAY - CL-CH			19	43	17	26		8
						18					14
	5					18					11
738.5			Stiff to very stiff, brown and gray, high plastic CLAY - CH			24					9
	10										
			with sand			16					13
	15										
						16					16
726.5	20		Boring terminated at 20 feet								
	25										

UNDRAINED SHEAR STRENGTH, tsf
○ HAND PENETROMETER
△ TORVANE
● UNCONFINED COMPRESSION
▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL
0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

LOG OF BORING NO. **B-3**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 20.0 ft

ELEVATION, ft	DEPTH, ft	SYMBOL	DESCRIPTION	SAMPLES	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	PERCENT PASSING NO. 200 SIEVE	SPT N-VALUE blows per foot
			SURFACE ELEVATION: 748.0ft								
748.0	0		Medium stiff, brown and gray, medium plastic CLAY - CL-CH			31					5
						26	41	15	26		8
	5					23					8
740.0			Stiff, brown and gray, high plastic CLAY - CH			19					11
	10										
			with sand			19					12
	15										
						20					14
728.0	20		Boring terminated at 20 feet								
	25										

UNDRAINED SHEAR STRENGTH, tsf
○ HAND PENETROMETER
△ TORVANE
● UNCONFINED COMPRESSION
▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL
0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

LOG OF BORING NO. **B-4**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 20.0 ft

ELEVATION, ft	DEPTH, ft	SYMBOL	DESCRIPTION	SAMPLES	DRY UNIT WEIGHT, PCF	NATURAL MOISTURE CONTENT, %	LIQUID LIMIT, %	PLASTIC LIMIT, %	PLASTICITY INDEX, %	PERCENT PASSING NO. 200 SIEVE	SPT N-VALUE blows per foot
			SURFACE ELEVATION: 748.0ft								
748.0	0		TOPSOIL - 4 inches								
747.8			Medium stiff to stiff, brown and gray, medium plastic CLAY - CL-CH			20					9
					99	21					
	5					26					7
						22					10
	10										
737.0			Stiff, brown and gray, high plastic CLAY - CH								
			trace sand and trace gravel			16					13
	15										
						16					14
728.0	20		Boring terminated at 20 feet								
	25										

UNDRAINED SHEAR STRENGTH, tsf
○ HAND PENETROMETER
△ TORVANE
● UNCONFINED COMPRESSION
▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL
0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

LOG OF BORING NO. **B-5**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 10.0 ft

SURFACE ELEVATION: 747.5ft

ELEVATION, ft	DEPTH, ft	DESCRIPTION	NATURAL MOISTURE CONTENT, %	SPT N-VALUE blows per foot
747.5	0	TOPSOIL - 4 inches		
747.3		Stiff to medium stiff, brown and gray, medium plastic CLAY - CL-CH	27	9
			15	20
742.5	5	Stiff, brown and gray, high plastic CLAY - CH trace gravel	23	12
			20	15
737.5	10	Boring terminated at 10 feet		
	15			
	20			
	25			

SAMPLES | DRY UNIT WEIGHT, PCF | LIQUID LIMIT, % | PLASTIC LIMIT, % | PLASTICITY INDEX, % | PERCENT PASSING NO. 200 SIEVE

UNDRAINED SHEAR STRENGTH, tsf
- ○ HAND PENETROMETER
- △ TORVANE
- ● UNCONFINED COMPRESSION
- ▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL

0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

LOG OF BORING NO. **B-6**

Cochran
530A East Independence
Union, Missouri 63084

PROJECT: Scenic Regional Library
LOCATION: Wright City
PROJECT NO.: 16-6414
DATE: 7-18-16 COMPLETION DEPTH : 10.0 ft

SURFACE ELEVATION: 747.0ft

ELEVATION, ft	DEPTH, ft	DESCRIPTION	NATURAL MOISTURE CONTENT, %	SPT N-VALUE blows per foot
747.0	0	TOPSOIL - 4 inches		
746.8		Stiff to medium stiff, brown and gray, medium plastic CLAY - CL-CH	22	9
			18	18
742.0	5	Stiff, brown and gray, high plastic CLAY - CH trace gravel	25	14
			25	9
737.0	10	Boring terminated at 10 feet		
	15			
	20			
	25			

SAMPLES
DRY UNIT WEIGHT, PCF
LIQUID LIMIT, %
PLASTIC LIMIT, %
PLASTICITY INDEX, %
PERCENT PASSING NO. 200 SIEVE

UNDRAINED SHEAR STRENGTH, tsf
○ HAND PENETROMETER
△ TORVANE
● UNCONFINED COMPRESSION
▲ UNCONSOLIDATED-UNDRAINED TRIAXIAL
0.5 1.0 1.5 2.0 2.5

WATER OBSERVATIONS:
NO FREE WATER ENCOUNTERED DURING DRILLING

BORING LOG: LEGEND & NOMENCLATURE

General Notes:

1. **Information on each boring log** is a compilation of subsurface conditions based on soil and/or rock classifications obtained from the field as well as from laboratory testing of the samples. The strata lines on the logs may be approximate or the transition between the strata may be gradual rather than distinct.
2. **Water level measurements** refer only to those observed at the time indicated and may vary with time, geologic condition or construction activity.

Drilling Method

HSA	Hollow-stem Auger
HA	Hand Auger
MR	Mud Rotary
SF	Solid Flight Auger

Sampling Method

PP	Pocket Penetrometer
GB	Grab Sample Taken From Auger Cuttings
TV	Torvane
CS	Continuous Sampler
ST	Three Inch Diameter Shelby Tube Sample (ASTM D 1587)
SS	Split Spoon Sample (Standard Penetration Test)
NX	NX Rock Core Sample; percent recovery and RQD reported (ASTM D 2113)

Standard Penetration Test – (SPT or N-value) is the standard penetration resistance based on the number of blows, using a 140-lb. Hammer with 30-inch free fall, required to drive a split spoon the last two of three, 6-inch drive increments. Driving is limited to 50 blows within any 6-inch interval. Samples which have not driven the full 6-inch interval upon-completing 50 blows are considered to have reached "split spoon refusal."

General Order of Classification Terms

Relative density or consistency * color * soil constituents * organics * odor * other

Density of Granular Soils

Descriptive Term	N-Value
Very Loose	0-4
Loose	5-10
Medium Dense	11-30
Dense	31-50
Very Dense	>50

Consistency of Fine-Grained Soils

Consistency	Undrained Shear Strength – Tons Per Square Ft.	Field Test	Approximate N-Value Range
Very Soft	less than 0.12	Thumb will penetrate soil more than 1"	0-1
Soft	0.13 to 0.25	Thumb will penetrate soil about 1"	2-4
Medium Stiff	0.26 to 0.50	Thumb will penetrate soil about ¼"	5-8
Stiff	0. 51 to 1.00	Thumb hardly indents soil	9-15
Very Stiff	1.01 to 2.00	Thumb will not indent soil, but readily Indented with thumbnail	16-30
Hard	greater than 2.00	Thumbnail will not indent soil	>30

Relative Composition

Trace	0-10%
With/Some	11-35%
Soil modifier such as Silty, clayey, sandy, etc.	>35%

Soil Grain Size

U.S. Standard Sieve

12"	3"	3/4"	4	10	40	200		
Boulders	Cobbles	Gravel		Sand			Silt	Clay
		Coarse	Fine	Coarse	Medium	Fine		
300	76.2	19.1	4.76	2.00	0.42	0.074	.002	

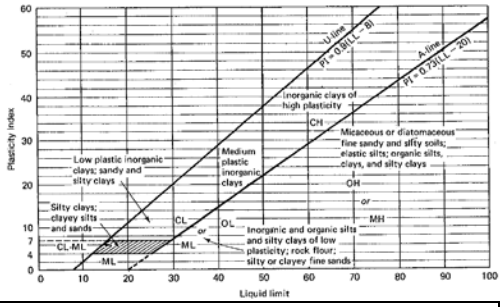
Soil Grain Size in Millimeters

Unified Soil Classification System

Soil Classifications of the samples are made by visual inspection and/or laboratory test results in accordance with the Unified Soil Classification System (ASTM Designations D-2487 and D-2488). Visual estimates are approximate only. If laboratory tests were performed to classify the soil, the unified designation is shown in parenthesis.

MAJOR DIVISIONS			SYMBOL	DESCRIPTION
Coarse-Grained Soils (more than 50% Larger than No. 200 Sieve Size)	Gravel and Gravelly Soils	Clean Gravels Little or No Fines	GW	Well-Graded Gravel, Gravel-Sand Mixture
			GP	Poorly-Graded Gravel, Gravel-Sand Mixture
		Gravels with Appreciable Fines	GM	Silty Gravel, Gravel-Sand-Silt Mixture
			GC	Clayey-Gravel, Gravel-Sand-Clay Mixture
	Sand and Sandy Soils	Clean Sands Little or No Fines	SW	Well-Graded Sand, Gravelly Sand
			SP	Poorly-Graded Sand, Gravelly Sand
		Sands with Appreciable Fines	SM	Silty Sand, Sand-Silt Mixture
			SC	Clayey Sand, Sand-Clay Mixture
Fine-Grained Soils (more than 50% Smaller than No. 200 Sieve Size)	Silts and Clays	Liquid Limit Less Than 50	ML	Silt, Clayey Silt, Silty or Clayey Very Fine Sand, Slight Plasticity
			CL	Clay, Sandy Clay, Silty Clay, Low to Medium Plasticity
			OL	Organic Silts or Silty Clays of Low Plasticity
	Silts and Clays	Liquid Limit More Than 50	MH	Silty, Fine Sandy or Silty Soil with High Plasticity
			CH	Clay, High Plasticity
			OH	Organic Clay or Medium to High Plasticity
	Highly Organic Soils		PT	Peat, Humus, Swamp Soil

PLASTICITY CHART



8 East Main Street
Wentzville, Missouri 63385
Telephone: 636-332-4574
Fax: 636-327-0760

737 Rudder Road
Fenton, Missouri 63026
Telephone: 314-842-4033
Fax: 314-842-5957

530A East Independence Drive
Union, Missouri 63084
Telephone: 636-584-0540
Fax: 636-584-0512
www.cochraneng.com

201B West Karsch Boulevard
Farmington, Missouri 63640
Telephone: 573-315-4810
Fax: 573-315-4811

905 Executive Drive
Osage Beach, Missouri 65065
Telephone: 573-525-0299
Fax: 573-525-0298